

X 4

PATENT
Case No. 659/920



I hereby certify that this correspondence is being deposited with the United States Postal Service with sufficient postage as first class mail in an envelope addressed to: Commissioner for Patents, Washington, D.C. 20231, on:

Marh 25, 2002
Date of Mailing

ANDREW D. STOVER, Reg. No. 38,629

Name of applicant, assignee or
Registered Representative

Signature

March 25, 2002
Date of Signature

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Application of:)	
)	
Richlen, et al.)	
)	
Serial No.: 10/032,701)	Group Art Unit No. 2185
)	
Filed: December 28, 2001)	
)	
For: ABSORBENT GARMENT HAVING A)	
WEAKENED REGION)	

PRELIMINARY AMENDMENT

Commissioner For Patents
Washington, D.C. 20231

Dear Sir:

Prior to examination, please enter the following preliminary amendment in the subject application.

IN THE SPECIFICATION:

Please rewrite the paragraph beginning at page 36, line 1 as follows:

For example, various trapezoidal tear and tensile strengths were determined for various samples of the body panel having a line of weakness formed therein by the various knife embodiments described above and as set forth in Table 1. As can be seen from the test results, the tear and tensile strength decreases as the perforation land area or width decreases. All of the webs tested were strong enough for the body panel web to flow through the process without breaking. In particular, webs with lines of weakness formed by four type of knives (embodiments 2, 3, 11 and 13) were tested, with 20 samples (3.0 inches wide) being tested for each knife. For comparison purposes, ten samples of the body panel taken across its entire length (6.37 inches (162 mm)) were also tested using the number 3 knife embodiment. As can be seen in Tables 2 and 3, the tear and tensile strengths increased for the larger sample. However, as explained above, it should be understood that the mean tensile and tear strength values for a body panel taken along its entire length that fall within the preferred ranges would also be encompassed within the scope of the invention, regardless of the sample size. Accordingly, where the body panel is not dimensioned to allow for a sample to be taken according to the procedure set forth below, the tear and tensile strength values can be determined for the entire length thereof and thereafter compared with the preferred values set forth in certain of the following claims.

Please rewrite the paragraph, including Tables II and III, beginning at page 37, line 9, as follows:

The test results are as follows:

TABLE 2 TRAPEZOIDAL TEAR STRENGTH					
	Knife 3	Knife 11	Knife 3	Knife 13	Knife 2
	Peak Load Gm	Peak Load Gm	Peak Load Gm	Peak Load Gm	Peak Load Gm
	4382.89	784.04	1084.43	2154.94	909.30
	7324.95	1417.30	1365.10	1076.31	1895.14
	3169.81	946.41	1137.78	1616.78	1723.49
	883.08	1020.64	1135.46	7951.70	832.75
	1385.05	872.18	1536.76	5028.96	1173.73
	3248.82	1343.07	1388.30	2361.39	1588.95
	1278.15	1185.33	1406.86	2055.19	821.15
	1947.43	883.78	1047.31	1697.97	888.42
	1171.25	1707.25	1945.01	1619.10	1704.93
	1633.71	888.42	1910.22	2131.74	1906.74
	987.66	1612.14	803.75	1442.81	1672.45
		2328.91	1812.79	2760.36	1391.78
		1558.79	1467.17	1890.50	953.37
		1742.04	1086.75	2277.88	670.37
		1519.36	847.83	1946.17	1540.24
		1482.24	1856.87	2421.70	1087.91
		1018.32	2130.58	1433.53	1554.15
		869.86	932.49	2959.85	1456.73
		1449.77	951.05	2066.79	1421.93
		1544.87	930.17	1744.36	6054.24
Mean (gm)	2492.07	1308.74	1338.83	2431.90	1562.39
(Force N/lbf)	24.42/5.42	12.82/2.88	13.12/2.95	23.83/5.36	15.31/3.44
Min (gm)	883.08	784.04	803.75	1076.31	670.37
Max (gm)	7324.95	2328.91	2130.58	7951.70	6054.24
Stdv	1956.86	399.64	409.24	1534.66	1124.63

**TABLE 3
TENSILE STRENGTH**

	Knife 3	Knife 11	Knife 3	Knife 13	Knife 2
	Peak Load Gm	Peak Load Gm	Peak Load Gm	Peak Load Gm	Peak Load Gm
	7261.04	3298.52	1867.30	4064.00	4523.28
	4328.27	2124.78	2192.05	4648.54	3377.38
	2720.13	3293.88	3692.85	6017.12	3535.12
	7456.25	1795.40	1549.51	2848.51	1535.60
	4923.19	3572.23	1936.89	6355.79	3395.94
	4253.91	1697.97	3112.95	3052.64	3001.60
	4444.47	2853.15	1584.31	3948.01	1637.66
	4588.55	2243.08	1941.53	3201.09	2412.42
	3988.98	2556.23	1649.26	3920.18	2166.54
	4453.77	3442.33	1735.08	4657.82	3015.52
	5076.57	1491.52	1472.97	3646.46	1974.01
		3256.76	2667.58	4704.21	1802.35
		2945.93	1871.94	5052.16	1340.75
		2282.52	1667.82	2257.00	1786.12
		3813.47	2052.87	4490.81	2356.75
		2043.60	2477.37	4486.17	1308.27
		2192.05	2434.45	5636.71	4198.53
		1229.40	1462.53	4346.99	2038.96
		2505.20	1636.50	3159.34	1319.87
		2212.93	1810.47	2417.06	1556.47
Mean (gm)	4863.20	2542.55	2040.81	4145.53	2414.16
(Force N/lbf)	47.66/10.71	24.92/5.60	20.00/4.50	40.63/9.14	23.66/5.32
Min (gm)	2720.13	1229.40	1462.53	2257.00	1308.27
Max (gm)	7456.25	3813.47	3692.85	6355.79	4523.28
Stdv	1376.79	736.45	581.67	1128.06	982.43

REMARKS:

The specification has been amended to use Arabic numerals to reference Tables 2 and 3, thereby maintaining consistency with Table 1. In addition, Tables 2 and 3 have been amended to properly identify the knife embodiments used to generate the data therein, as set forth at page 36, lines 16-21. A marked-up version of the specification

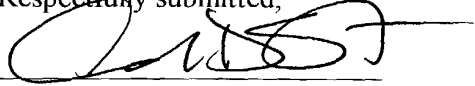
showing the changes thereto is provided at Appendix A attached hereto. No new matter has been added to the above-referenced application by way of this preliminary amendment. Any questions resulting from this preliminary amendment should be directed to Applicants' undersigned attorney at 312-321-4200.

Dated: March 25, 2002

BRINKS HOFER GILSON & LIONE LTD.
Post Office Box 10395
Chicago, Illinois 60610
(312) 321-4200

Respectfully submitted,

By:


Andrew D. Stover
Reg. No. 38,629
Attorney for Applicants

APPENDIX A

The paragraph beginning at page 36, line 1 has been amended as follows:

For example, various trapezoidal tear and tensile strengths were determined for various samples of the body panel having a line of weakness formed therein by the various knife embodiments described above and as set forth in Table 1. As can be seen from the test results, the tear and tensile strength decreases as the perforation land area or width decreases. All of the webs tested were strong enough for the body panel web to flow through the process without breaking. In particular, webs with lines of weakness formed by four type of knives (embodiments 2, 3, 11 and 13) were tested, with 20 samples (3.0 inches wide) being tested for each knife. For comparison purposes, ten samples of the body panel taken across its entire length (6.37 inches (162 mm)) were also tested using the number 3 knife embodiment. As can be seen in Tables [II and III] 2 and 3, the tear and tensile strengths increased for the larger sample. However, as explained above, it should be understood that the mean tensile and tear strength values for a body panel taken along its entire length that fall within the preferred ranges would also be encompassed within the scope of the invention, regardless of the sample size. Accordingly, where the body panel is not dimensioned to allow for a sample to be taken according to the procedure set forth below, the tear and tensile strength values can be determined for the entire length thereof and thereafter compared with the preferred values set forth in certain of the following claims.

The paragraph, including Tables II and III, beginning at page 37, line 9, has been amended as follows:

The test results are as follows:

TABLE [II] 2 TRAPEZOIDAL TEAR STRENGTH				
Knife [4] 3	Knife [12] 11	Knife [4] 3	Knife [14] 13	Knife [3] 2
Peak Load Gm	Peak Load Gm	Peak Load Gm	Peak Load Gm	Peak Load Gm
4382.89	784.04	1084.43	2154.94	909.30
7324.95	1417.30	1365.10	1076.31	1895.14
3169.81	946.41	1137.78	1616.78	1723.49
883.08	1020.64	1135.46	7951.70	832.75
1385.05	872.18	1536.76	5028.96	1173.73
3248.82	1343.07	1388.30	2361.39	1588.95
1278.15	1185.33	1406.86	2055.19	821.15
1947.43	883.78	1047.31	1697.97	888.42
1171.25	1707.25	1945.01	1619.10	1704.93
1633.71	888.42	1910.22	2131.74	1906.74
987.66	1612.14	803.75	1442.81	1672.45
	2328.91	1812.79	2760.36	1391.78
	1558.79	1467.17	1890.50	953.37
	1742.04	1086.75	2277.88	670.37
	1519.36	847.83	1946.17	1540.24
	1482.24	1856.87	2421.70	1087.91
	1018.32	2130.58	1433.53	1554.15
	869.86	932.49	2959.85	1456.73
	1449.77	951.05	2066.79	1421.93
	1544.87	930.17	1744.36	6054.24
Mean (gm)	2492.07	1308.74	2431.90	1562.39
(Force N/lbf)	24.42/5.42	12.82/2.88	23.83/5.36	15.31/3.44
Min (gm)	883.08	784.04	1076.31	670.37
Max (gm)	7324.95	2328.91	7951.70	6054.24
Stdv	1956.86	399.64	1534.66	1124.63

**TABLE [III] 3
TENSILE STRENGTH**

	Knife [4] <u>3</u>	Knife [12] <u>11</u>	Knife [4] <u>3</u>	Knife [14] <u>13</u>	Knife [3] <u>2</u>
	Peak Load Gm	Peak Load Gm	Peak Load Gm	Peak Load Gm	Peak Load Gm
	7261.04	3298.52	1867.30	4064.00	4523.28
	4328.27	2124.78	2192.05	4648.54	3377.38
	2720.13	3293.88	3692.85	6017.12	3535.12
	7456.25	1795.40	1549.51	2848.51	1535.60
	4923.19	3572.23	1936.89	6355.79	3395.94
	4253.91	1697.97	3112.95	3052.64	3001.60
	4444.47	2853.15	1584.31	3948.01	1637.66
	4588.55	2243.08	1941.53	3201.09	2412.42
	3988.98	2556.23	1649.26	3920.18	2166.54
	4453.77	3442.33	1735.08	4657.82	3015.52
	5076.57	1491.52	1472.97	3646.46	1974.01
		3256.76	2667.58	4704.21	1802.35
		2945.93	1871.94	5052.16	1340.75
		2282.52	1667.82	2257.00	1786.12
		3813.47	2052.87	4490.81	2356.75
		2043.60	2477.37	4486.17	1308.27
		2192.05	2434.45	5636.71	4198.53
		1229.40	1462.53	4346.99	2038.96
		2505.20	1636.50	3159.34	1319.87
		2212.93	1810.47	2417.06	1556.47
Mean (gm)	4863.20	2542.55	2040.81	4145.53	2414.16
(Force N/lbf)	47.66/10.71	24.92/5.60	20.00/4.50	40.63/9.14	23.66/5.32
Min (gm)	2720.13	1229.40	1462.53	2257.00	1308.27
Max (gm)	7456.25	3813.47	3692.85	6355.79	4523.28
Stdv	1376.79	736.45	581.67	1128.06	982.43